

## **Analysis of Order of Stress Singularity at a Vertex in 3D Transversely Isotropic Piezoelectric Dissimilar Bonded Joints**

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### **Abstract**

*The order of singularity near the vertex of bonded joints is one of the main factors responsible for debonding under mechanical or thermal loading. The distribution of stress singularity field near the vertex of bonded joints is very important to maintain the reliability of intelligent materials. In this paper, order of stress singularity at a vertex in 3D transversely isotropic piezoelectric dissimilar bonded joints is analyzed. Eigen analysis based on FEM is used for stress singularity field analysis of piezoelectric bonded joints. The Eigen equation is used for calculating the order of stress singularity, and the angular function. The numerical result shows that the angular functions have larger value near the interface edge than the inner portion of the joint. From the numerical result, it was observed that the possibility of debonding at the interface edge of the piezoelectric bonded joints, due to the higher stress concentration at the free edge.*

**Keywords:** Piezoelectric Bonded Joints, Order of Singularity, Transversely Isotropic Material, Smart Structures, Eigen Analysis.

### **1. Introduction**

Piezoelectric materials are being widely used in the electronics industry due to their high functionality. Mechanical stress occurs in piezoelectric material for any electric input. The stress concentrations caused by mechanical or electric loads may lead to crack initiation and extension, and sometimes the stress concentrations may be high enough to fracture the material parts. In the case of multilayer piezoelectric stacks, the electrodes that terminate inside the material body are a source of electric field, which can result in high stress concentrations. Reliable service lifetime predictions of piezoelectric components demand a complete understanding of the debonding processes of these materials. Industrial products such as electronic devices and heat endurance parts are composed of dissimilar materials. A mismatch of material properties causes a failure at the free edge of joint, because a stress concentration occurs along the free edge of interface especially at the vertex of joints [1].

Sosa has suggested a general method of solving plane problems of piezoelectric media with defects [2]. Zak and Williams used Eigen functions for analyzing stress singularity field at a crack tip perpendicular to a bimaterial interface. They found that a real part of Eigen value is within the range of 0 to 1, and expressed a relationship between stress distribution and the order of stress singularity at the crack tip [3]. Aksentian determined Eigen values and Eigen vectors at the singular point in plane intersecting a free edge of the interface in three dimensional dissimilar joints [4]. Yamada and Okumura developed a finite element analysis for solving Eigen value equation to determine directly the order of stress singularity and the angular variation of the stress and displacement fields [5]. Pageau and Biggers determined the order of stress singularity and the angular variation of the displacement and the stress fields around the singular points in plane intersecting a wedge front in the three-dimensional anisotropic material structures using the two dimensional displacement formulation under a plane strain assumption [6].

Thus, at present, no clear picture exists of the effects of stress singularity field near the vertex of three-dimensional transversely isotropic piezoelectric dissimilar bonded joints. Therefore, the purpose of this analysis is to obtain a better understanding of the effect of stress singularity field near the vertex of transversely isotropic

piezoelectric bimaterial joints on interface. In this study, three-dimensional FEM Eigen equation was formulated for analyzing the order of singularity in piezoelectric bimaterial joints.

## 2. Formula of Analysis

In the absence of body forces and free charges, the equilibrium equations of piezoelectric materials are expressed as follows [7]:

$$\sigma_{ij,j} = 0 \quad (1)$$

$$d_{i,i} = 0 \quad (2)$$

where  $\sigma_{ij}$  represents the stress and  $d_i$  the electric displacement.

The constitutive relations are shown as follows:

$$\sigma_{ij} = c_{ijkl}\epsilon_{kl} - e_{kij}E_k \quad (3)$$

$$d_i = e_{ikl}\epsilon_{kl} + \chi_{ik}E_k \quad (4)$$

where  $c_{ijkl}$  is the elastic constant,  $e_{ikl}$  and  $\chi_{ik}$  are the piezoelectric constant and electric permittivity (dielectric constant), respectively.

The elastic strain-displacement and electric field-potential relations are presented as follows:

$$\epsilon_{ij} = \frac{1}{2}(u_{j,i} + u_{i,j}) \quad (5)$$

$$E_i = -\psi_{,i} \quad (6)$$

where  $\epsilon_{ij}$  is the strain, and  $E_i$  is the electric field.  $u_i$  is the elastic displacement and  $\psi$  is the electric potential.

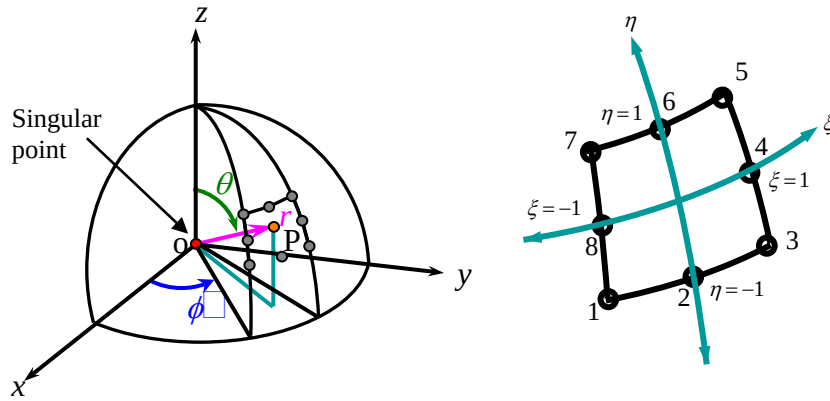


Fig.1 Element geometry and natural co-ordinates at a free edge singular point

Figure 1 represents the geometry of a typical case where a singular stress state occurs at the point o. The region surrounding the singular point is divided into a number of quadratic pyramidal elements with a summit o, with each element being located in spherical co-ordinates  $r$ ,  $\theta$ , and  $\phi$  by its nodes 1 to 8. A point P in the element can be located using the singular transformation by the relations.

$$r = r_o \left( \frac{1+\alpha}{2} \right)^{1/p} \quad \text{or,} \quad \rho = \frac{r}{r_o} = \left( \frac{1+\alpha}{2} \right)^{1/p}$$

$$\theta = \sum_{i=1}^8 H_i \theta_i \quad \text{and} \quad \phi = \sum_{i=1}^8 H_i \phi_i \quad (7)$$

where,

$$H_1 = -\frac{1}{4}(1-\eta)(1-\xi)(\eta+\xi+1) \quad H_2 = \frac{1}{2}(1-\eta)(1-\xi^2)$$

$$H_3 = -\frac{1}{4}(1-\eta)(1+\xi)(-\eta+\xi-1) \quad H_4 = \frac{1}{2}(1-\eta^2)(1+\xi)$$

$$H_5 = \frac{1}{4}(1+\eta)(1+\xi)(\eta+\xi-1) \quad H_6 = \frac{1}{2}(1+\eta)(1-\xi^2)$$

$$H_7 = \frac{1}{4}(1+\eta)(1-\xi)(\eta-\xi-1) \quad H_8 = \frac{1}{2}(1-\eta^2)(1-\xi)$$

$\theta$  and  $\phi$  are the nodal values of the angular co-ordinates and  $\alpha$ ,  $\eta$ , and  $\xi$  are natural co-ordinates of the element whose ranges are shown in Fig.1.  $H$  interpolation function,  $p$  Eigen value,  $\rho = r/r_o$ ,  $r$  the distance from the singular point. The elastic displacement and electric potential relations are:

$$(\bar{u} - \bar{u}_o) = \left( \frac{1+\alpha}{2} \right) \left[ \sum_{i=1}^8 H_i (\bar{u}_i - \bar{u}_o) \right] \quad (8)$$

$$(\bar{\psi} - \bar{\psi}_o) = \left( \frac{1+\alpha}{2} \right) \left[ \sum_{i=1}^8 H_i (\bar{\psi}_i - \bar{\psi}_o) \right] \quad (9)$$

where  $\bar{u}_o$  and  $\bar{u}$  is the elastic displacement at o and P, respectively, and  $\bar{\psi}_o$  and  $\bar{\psi}$  is the electric potential at o and P, respectively.

$$u = (\bar{u} - \bar{u}_o), \quad u_i = (\bar{u}_i - \bar{u}_o) \quad (10)$$

$$\psi = (\bar{\psi} - \bar{\psi}_o), \quad \psi_i = (\bar{\psi}_i - \bar{\psi}_o) \quad (11)$$

From the above equation, the elastic displacement and electric potential relations are expressed as follows:

$$u_k = \rho^p \left[ \sum_{i=1}^8 H_i u_{ki} \right] \quad (k = r, \theta, \phi) \quad (12)$$

$$\psi = \rho^p \left[ \sum_{i=1}^8 H_i \psi_i \right] \quad (13)$$

### 3. Problem Description and Numerical Example

For a transversely isotropic piezoelectric material, taking  $z$  to be parallel to the poling axis of the material, by convention, the constitutive relation is expressed in the following form:

$$\{\sigma\} = [c]\{\varepsilon\} - [e]\{E\} \quad \text{and} \quad \{d\} = [e]^T \{\varepsilon\} + [\chi]\{E\} \quad (14)$$

where  $\{\sigma\}$  and  $\{\varepsilon\}$  are the stress and strain which are the mechanical field variables,  $\{d\}$  and  $\{E\}$  are the electric displacement and electric field, respectively,  $[c]$  is the elastic constant, and  $[e]$  and  $[\chi]$  are the piezoelectric constant and electric permittivity (dielectric constant) respectively.

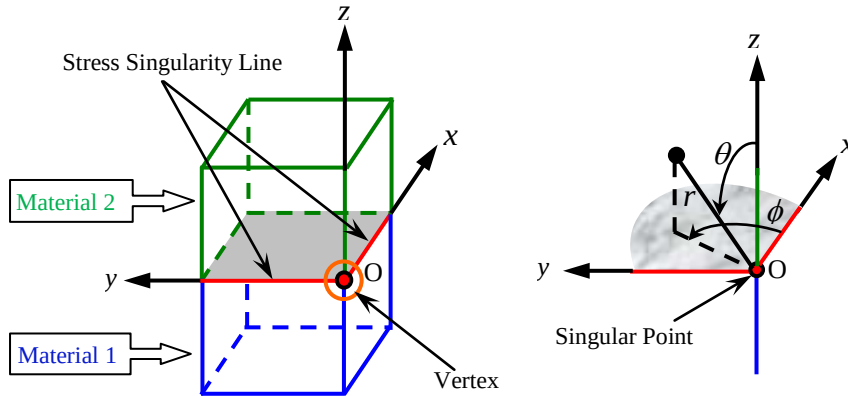


Fig. 2 Singular point of 3D piezoelectric dissimilar bonded joint in x, y, z plane

Table1: Material properties of piezoelectric materials

| Material | Elastic Constant, $10^{10}$ N/m <sup>2</sup> |                 |                 |                 |                 | Piezoelectric Constant, C/m <sup>2</sup> |                 |                 | Dielectric Constant, $10^{-10}$ C/Vm |                 |
|----------|----------------------------------------------|-----------------|-----------------|-----------------|-----------------|------------------------------------------|-----------------|-----------------|--------------------------------------|-----------------|
|          | C <sub>11</sub>                              | C <sub>12</sub> | C <sub>13</sub> | C <sub>33</sub> | C <sub>44</sub> | e <sub>15</sub>                          | e <sub>31</sub> | e <sub>33</sub> | χ <sub>11</sub>                      | χ <sub>33</sub> |
| PZT-5H   | 12.6                                         | 5.50            | 5.30            | 11.7            | 3.53            | 17.0                                     | -6.50           | 23.3            | 151.0                                | 130.0           |
| PZT-5A   | 12.1                                         | 7.54            | 7.52            | 11.3            | 2.11            | 12.3                                     | -5.20           | 15.8            | 81.1                                 | 73.5            |

The Eigen equation is formulated for determining the order of stress singularity as follows.

$$(p^2 [\mathbf{A}] + p[\mathbf{B}] + [\mathbf{C}])\{\mathbf{U}\} = \{\mathbf{0}\} \quad (15)$$

Where  $p$  represents the characteristic root, which is related to the order of singularity,  $\lambda$ , as  $\lambda=1-p$ .  $[\mathbf{A}]$ ,  $[\mathbf{B}]$  and  $[\mathbf{C}]$  are matrices composed of material properties, and  $\{\mathbf{U}\}$  represents the elastic displacement and electric potential vector.

The elastic displacement and electric potential equation is expressed by the following equation.

$$u_j(r, \theta, \phi) = b_j(\theta, \phi)r^{1-\lambda} \quad (16)$$

$$\psi(r, \theta, \phi) = q(\theta, \phi)r^{1-\lambda} \quad (17)$$

By differentiating the above two equations, get the angular function of strain and electric field equation respectively. The stress and electric displacement distribution equations in the stress singularity region can be expressed as follows.

$$\sigma_{ij}(r, \theta, \phi) = K_{ij}r^{-\lambda} f_{ij}(\theta, \phi) \quad (18)$$

$$d_i(r, \theta, \phi) = F_i r^{-\lambda} l_i(\theta, \phi) \quad (19)$$

Where  $r$  represents the distance from the stress singular point,  $b_j(\theta, \phi)$  the angular function of elastic displacement,  $q(\theta, \phi)$  the angular function of electric potential,  $f_{ij}(\theta, \phi)$  the angular function of stress distribution,  $l_i(\theta, \phi)$  the angular function of electric displacement,  $K_{ij}$  the intensity of singularity,  $F_i$  the intensity of electric field, and  $\lambda$  the order of stress singularity. Angular functions of stress components obtained from Eigen analysis in Eq. (15) are examined.

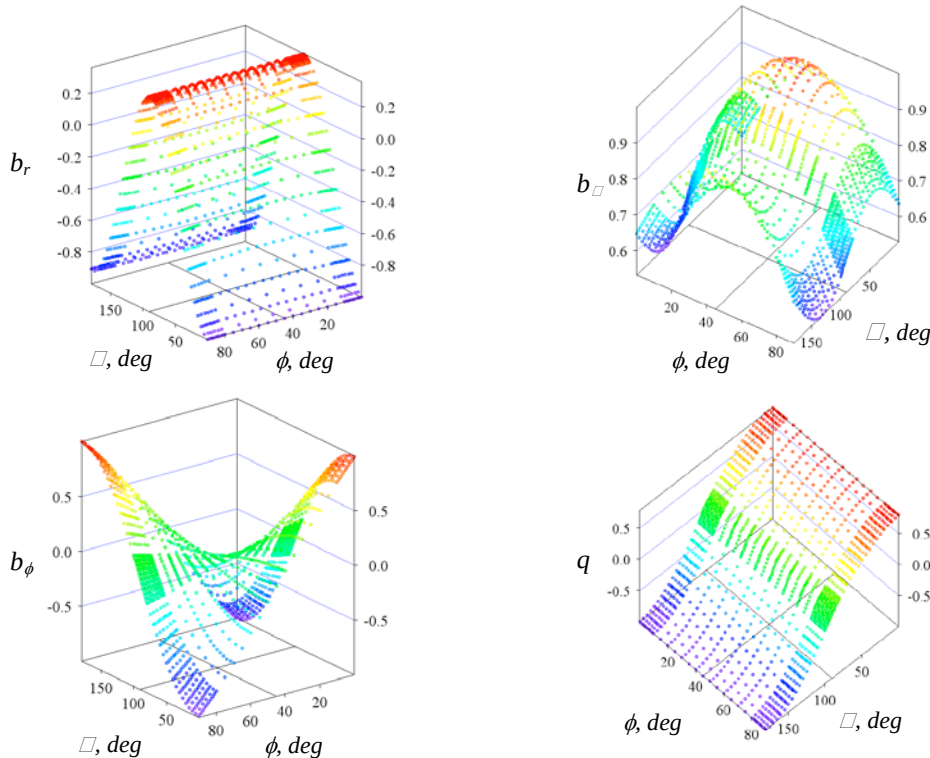


Fig. 3 Distribution of  $b_i$  &  $q$  against angle  $\phi$  and  $\theta$

The distributions of elastic displacement and electric potential are shown in fig. 3. It is found that, the angular function of elastic displacement and electric potential is continuous at the interface of the joints and has larger value at the free edge than the inner portion. So there is a possibility to debond near the free edge of the joint. It is also found that the angular function of elastic displacement and electric potential at  $\phi = 0^\circ$  is agreed with that at  $\phi = 90^\circ$ . The figure of  $b_\theta$  and  $b_r$  is symmetry with respect to  $\phi$  and the figure of  $b_\phi$  and  $q$  is antisymmetry with respect to  $\phi$ . The distributions of normalized angular function of strain and electric field with respect to the angle  $\phi$  at  $\theta = 90^\circ$  in the singular field for the piezoelectric bonded structure are shown in fig. 4. It is shown from the figure that the strain and electric field have larger value near the free edge of the bonded joints.

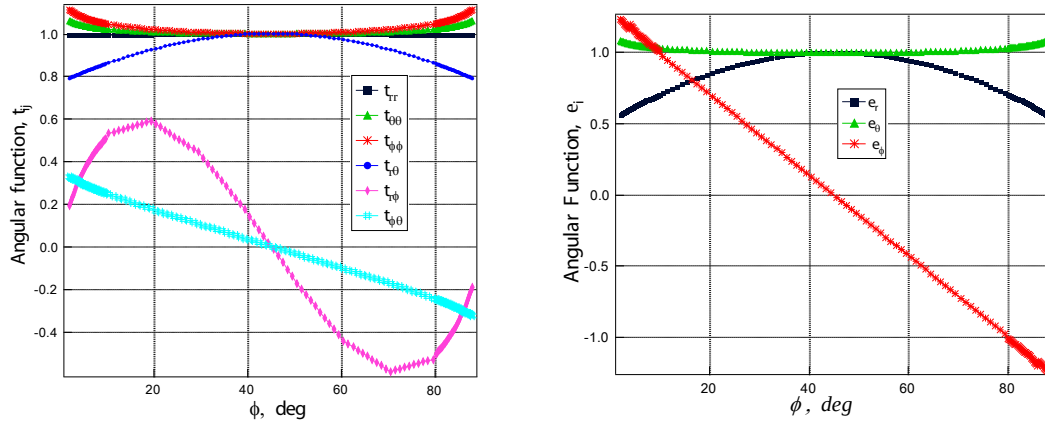


Fig. 4 Distribution of normalized angular function of strain and electric field against  $\phi$  at  $\theta = 90^\circ$

The distributions of normalized angular function of stress and electric displacement with respect to the angle  $\phi$  at  $\theta = 90^\circ$  for the piezoelectric bonded structure are shown in fig. 5. These distributions are nearly similar to the distribution of angular function strain and electric field. It is shown from the figure that the stress and electric displacement have larger value near the free edge of the bonded joints. So there is another possibility to debond and delamination occurs near the free edge of the bonded joints.

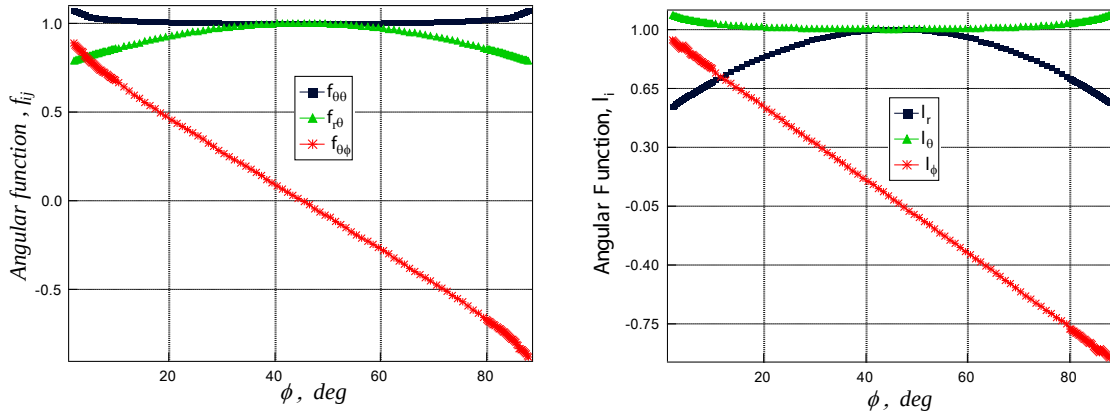


Fig. 5 Distribution of normalized angular function of stress and electric displacement against  $\phi$  at  $\theta = 90^\circ$

#### 4. Conclusion

In this paper, a finite element method formulation near the vertex of transversely isotropic piezoelectric dissimilar bonded joints was presented. Angular functions for singularity corner were derived from Eigen

analysis using a finite element method. From the numerical result, the following conclusions can be drawn for the piezoelectric bimaterial joints.

- a) The higher angular function occurs at the free edge of the material joint than the inner portion of the joint.
- b) The possibility to debond and delamination at the edge of the transversely isotropic piezoelectric dissimilar bonded joints was due to the higher stress and electric displacement concentration at the free edge.

## **5. References**

- [1] W. Attaporn, and H. Koguchi, "Intensity of stress singularity at a vertex and along the free edges of the interface in 3D-dissimilar material joints using 3D-enriched FEM", *CMES*, Vol. 39, No. 3, pp. 237-262, 2009.
- [2] H. A. Sosa, "Plane problems in piezoelectric media with defects", *International Journal of Solids and Structure*, Vol. 28, pp.491-505, 1991.
- [3] A. R. Zak, and M. L. Williams, "Crack point stress singularities at a bi-material interface", *Journal of Applied Mechanics*, Brief Notes, pp.142-143, 1963.
- [4] O. K. Aksentian, "Singularities of the stress-strain state of a plate in the neighborhood of an edge", *PMM*, Vol. 31, No. 1, pp.178-186, 1967.
- [5] Y. Yamada, and H. Okumura, "Analysis of local stress in composite materials by 3-D finite element", *Proceeding of the Japan-U.S. Conference*, Tokyo, pp. 55-64, 1981.
- [6] S. S. Pageau, and Jr. S. B. Biggers, "A finite element approach to three-dimensional singular stress states in anisotropic multi-material wedges and junctions", *International Journal of Solids and Structure*, Vol. 33, pp. 33-47, 1996.
- [7] K. M. Liew, and J. Liang, "Modeling of 3D piezoelectric and elastic bimaterials using the boundary element method", *Computational Mechanics*, Vol. 29, pp. 151-162, 2002.